



Axi $\psi - \omega$ Eqs.

(ALE-FE Conjugated Heat-Transfer)

$$\frac{\partial \omega_z}{\partial t} + \mathbf{c} \cdot \nabla \omega_z = \frac{\omega_z v_r}{r} + \frac{1}{\text{Re}} \left[\frac{\partial}{\partial r} \left(\frac{1}{r} \frac{\partial r \omega_z}{\partial r} + \frac{\partial^2 \omega_z}{\partial z^2} \right) \right]$$

$$\frac{\partial}{\partial r} \left(\frac{1}{r} \frac{\partial \psi}{\partial r} \right) + \frac{\partial^2}{\partial z^2} \left(\frac{\psi}{r} \right) = -\omega_z$$

$$\frac{\partial T}{\partial t} + \mathbf{c} \cdot \nabla T = \frac{1}{\text{RePr}} \left[\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial T}{\partial r} \right) + \frac{\partial^2 T}{\partial z^2} \right]$$

Auxiliary:

$$\mathbf{v} = (v_z, v_r) \\ = \left(\frac{1}{r} \frac{\partial \psi}{\partial r}, -\frac{1}{r} \frac{\partial \psi}{\partial z} \right)$$

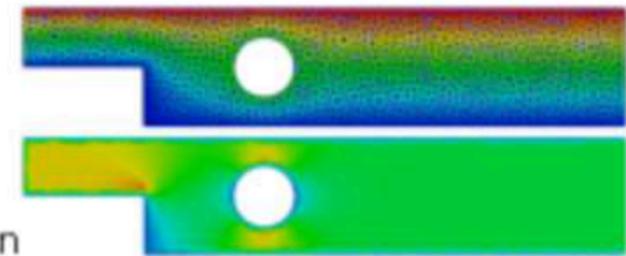
$$\omega_z = \frac{\partial v_r}{\partial z} - \frac{\partial v_z}{\partial r}$$

$$\text{ALE formulation: } \frac{\partial \omega_z}{\partial t} + (\mathbf{v} - \hat{\mathbf{v}}) \cdot \nabla \omega_z \begin{cases} \hat{\mathbf{v}} = \mathbf{v} \rightarrow \text{Lagrangian} \\ \hat{\mathbf{v}} = \mathbf{0} \rightarrow \text{Eulerian} \end{cases}$$

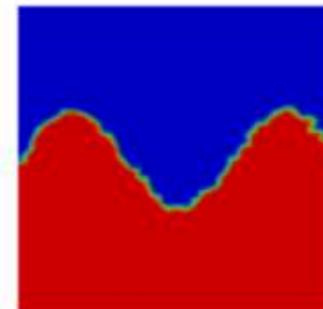


Validations

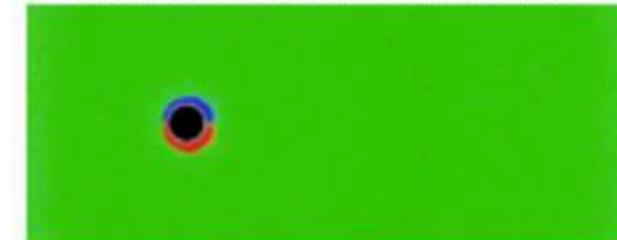
2D Backward facing
step with hole



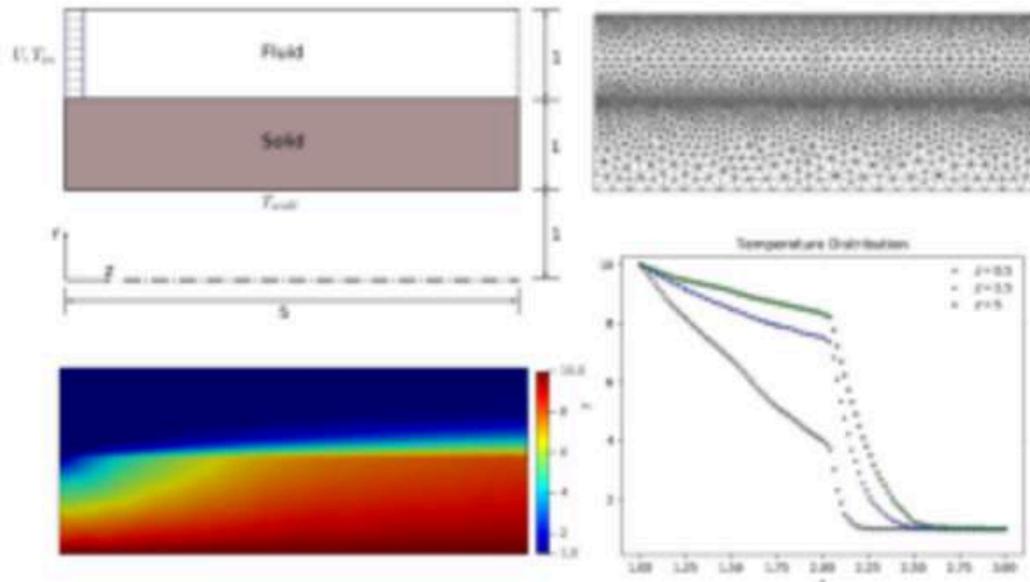
2D Natural Convection



2D Vortex-Induced Vibration



Results for Axisymmetric Conjugated Heat Transfer



Axi Navier-Stokes Eqs.

(ALE-FE 2-phase flows)

$$\rho(\mathbf{x}) \left[\frac{\partial \mathbf{v}}{\partial t} + \mathbf{c} \cdot \nabla \mathbf{v} \right] = -\nabla p + \frac{1}{N^{1/2}} \nabla \cdot \mu(\mathbf{x}) [\nabla \mathbf{v} + \nabla \mathbf{v}^T] + \rho(\mathbf{x}) \mathbf{g} + \frac{1}{E_0} \mathbf{f}_{st}$$

$$\nabla \cdot \mathbf{v} = 0$$

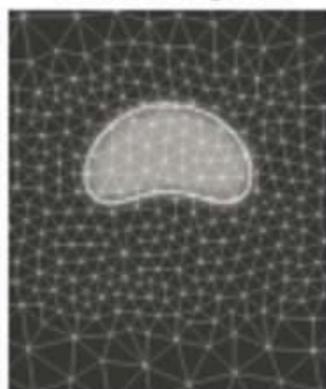
$$\text{where: } \nabla^T = \left[\frac{\partial}{\partial r}; \frac{\partial}{\partial x} \right] \quad \nabla \cdot = \left[\frac{1}{r} \frac{\partial}{\partial r} r; \frac{\partial}{\partial x} \right] \quad \mathbf{f}_{st} = \kappa n \delta$$

$$\text{ALE formulation: } \frac{\partial \mathbf{v}}{\partial t} + (\mathbf{v} - \hat{\mathbf{v}}) \cdot \nabla \mathbf{v} \begin{cases} \hat{\mathbf{v}} = \mathbf{v} \rightarrow \text{Lagrangian} \\ \hat{\mathbf{v}} = \mathbf{0} \rightarrow \text{Eulerian} \end{cases}$$

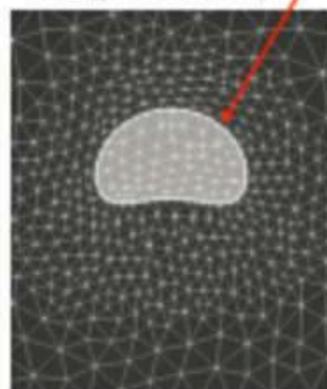


Interface definition

Uncoupled approach
(interface and background mesh **disconnected**)
*Level-Set, VOF, Inter. Tracking, ALE



Coupled approach
(interface and background mesh **connected**)
Lagrangian, *ALE (present work)



sharp transition across phases for fluid properties

surface tension calculation (Frenet-Serret)

$$\kappa_{2D} \vec{n} = \frac{d\vec{t}}{ds} \approx \frac{\vec{t}_2 - \vec{t}_1}{\Delta s}$$

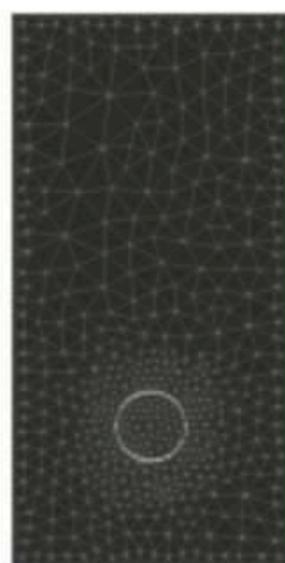
$$\kappa = \kappa_{2D} + \frac{1}{R} = \kappa_{2D} + \frac{\sin(\alpha)}{r}$$



The method in action

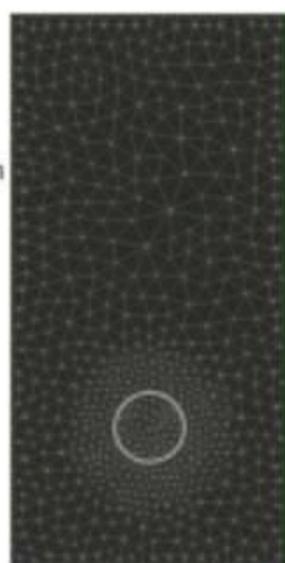
Uncoupled approach

- smooth transition
- more nodes are required
- implicit location of interface



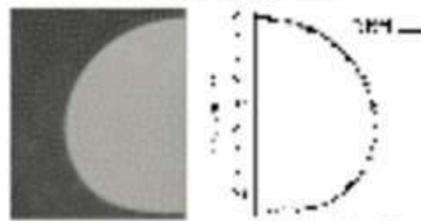
Coupled approach

- sharp transition
- Lagrangian motion of interface
- remeshing is required
- explicit location of interface

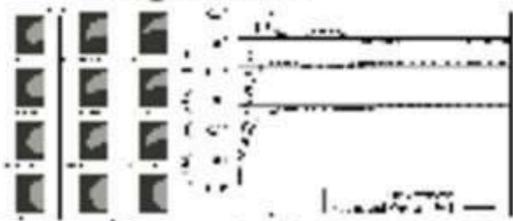


Validations

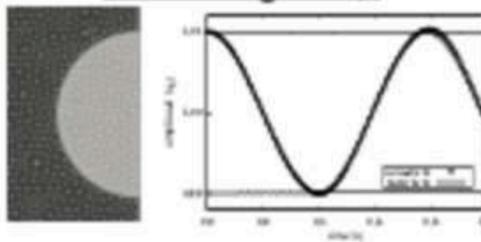
sessile drop



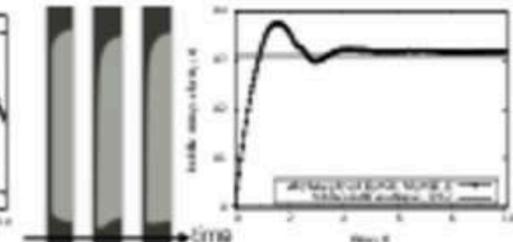
rising bubble



oscillating drop

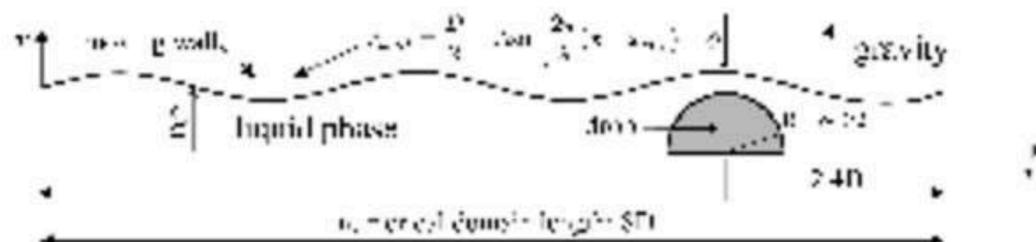


rising Taylor bubble



Geometries

Corrugated channel



$$\text{wall moves as: } r_{wall} = \frac{D}{2} + A \sin \left\{ \frac{2\pi}{\lambda} (x + x_{ref}) - \phi \right\}$$

where x_{ref} is bubble's nose position



Properties limits

system	μ_{out} (Pa.s)	μ_{in} (Pa.s)	ρ_{out} (kg/m ³)	ρ_{in} (kg/m ³)	σ (N/m)	ω (Hz)	N [-]	Eu [-]	Mo [-]
GW1	450E-3	238E-3	1250	967	0.0240	25.30	75.7	51.1	23.3
GW3	450E-3	530E-3	1250	965	0.0105	0.01	75.7	116.8	277.9
GW5	450E-3	97E-3	1250	950	0.0057	12.30	75.7	49.1	20.6
GW8	450E-3	007E-3	1250	903	0.0250	25.63	75.7	49.1	20.6
WG1	190E-3	238E-3	1230	967	0.0230	24.85	411.1	52.5	0.8
WG2	67E-3	83E-3	1200	970	0.0019	7.18	3146.9	619.6	24.0
WG4	93E-3	104E-3	1220	990	0.0257	26.15	1688.2	46.6	0.04
DEGG3	28E-3	530E-3	1110	965	0.0032	9.41	15416.9	340.3	0.16
DEGG10	28E-3	63E-3	1110	975	0.0016	6.09	15416.9	680.6	1.33
DEGG11	87E-3	157E-3	1160	968	0.0050	11.74	1744.0	227.6	3.8
DEGG12	87E-3	115E-3	1160	966	0.0042	10.76	1744.0	270.9	6.53

spherical bubble frequency: $\omega^2 = \frac{n(n+1)(n-1)(n+2)\sigma}{[(n+1)\rho_{in} + n\rho_{out}]R^3}$

U. Olgac, A. D. Kayaalp, M. Muradoglu 2006

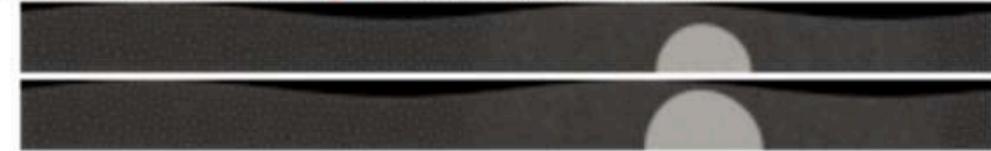
M. Hemmat & A. Borhan, 1996



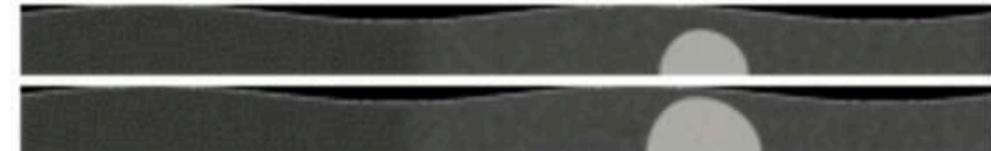
Results for $A=0.07D$

(I)

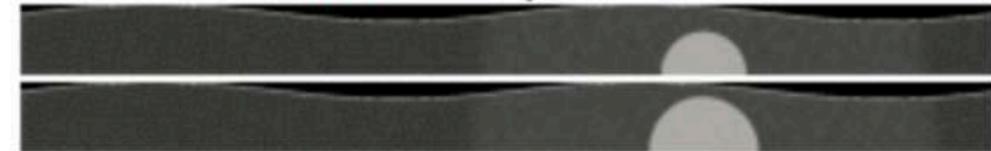
GW3: $\kappa = \{0.78, 0.97\}$, higher viscosity for outer fluid



DEGG 12: $\kappa = \{0.73, 0.95\}$

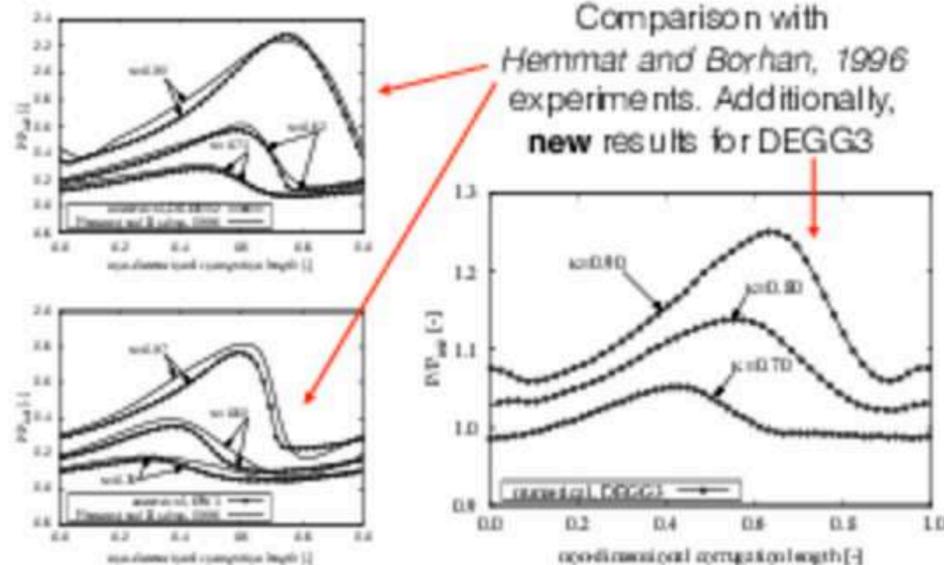


DEGG3: $\kappa = \{0.70, 0.90\}$, lower viscosity for outer fluid



Comparisons

(II)



Results

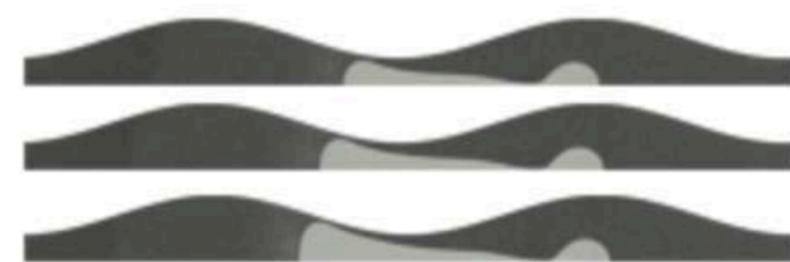
(III)

DEGG 12: $\kappa = \{0.73, 0.82, 0.95\}$

$A=0.14$



$A=0.21$





Conclusions/**Further steps**/**Key points**

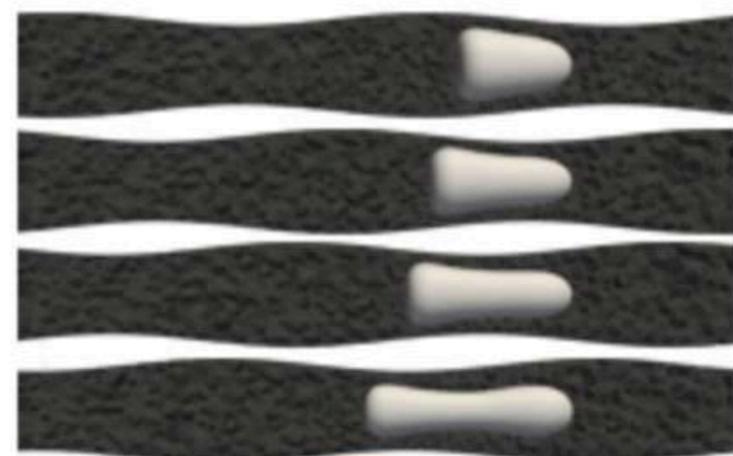
- moving mesh/boundary technique facilitates study of **periodic** and **very long** geometries and can be easily extend to any ALE CFD method
 - study about bubble dynamics in two-phase systems with long periodic channels;
 - numerics evaluated several flow parameters as bubble shape, capillary effects, bubble velocity and liquid film thickness;
 - bubble's resonance frequency vs channel pattern;
 - effects of oscillation and perturbation on bubble's path;
 - 2-phase fluid-structure interactions.
- when does bubble break up in corrugated channels occur?
 - is CFD a reasonable approach for modeling bubble **breakup/coalescence**?



Thanks!

on-going
3D
simulations

time



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